



Locomotion

R. Siegwart and I. R. Nourbakhsh, Thomas W. Kenny, "Introduction to Autonomous Mobile Robots," The MIT Press 2004 PowerPoint 中部分圖片擷取和修改自教科書和網路圖片

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Key Questions

- □ The three key questions in Mobile Robotics
 - Where am I?
 - Where am I going?
 - How do I get there?
- □ To answer these questions, the robot has to
 - Be able to "move"
 - Have a model of the environment (given or autonomously built)
 - Perceive and analyze the environment
 - Find its position within the environment
 - Plan and execute the movement



Mobile Robots with Wheels

- Wheels are the straight forward solutions for most applications
- □ Three wheels are sufficient to guarantee stability
 - With more than three wheels, a flexible suspension is required
- Selection of wheels depends on the application

Idealized Rolling Wheels

- Assumptions
 - Rigid wheel
 - No side slip
 - In the direction orthogonal to that of rolling
 - No translational slip
 - between the wheel and the floor
- For low velocity, idealized rolling is a reasonable wheel model
- Parameters
 - r: radius
 - v: linear velocity
 - w: angular velocity
 - t: steering velocity

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P.S. An interesting Research

- □ Gyrover
 - A single-wheel, gyroscopically stabilized robot







Four Basic Wheels Types -2

- □ c) Swedish wheel
 - Three degrees of freedom; rotation around the (motorized) wheel axle, around the rollers and around the contact point



d) Spherical wheel







With parameters







Four Basic Wheels Types -5



- Velocity of point P

V= $(\mathbf{r} \times \mathbf{w})\mathbf{a}_{\mathbf{x}}$

where, $\begin{array}{c} \mathbf{ax} : \mathbf{A} \text{ unit vector of } \mathbf{x} \text{ axis} \\ \mathbf{ay} : \mathbf{A} \text{ unit vector of } \mathbf{y} \text{ axis} \end{array}$

- Restriction to the robot mobility







Swedish wheel

Velocity of point P

 $v = (r \times w)a_x + Ua_s$

where, ax: A unit vector of x axis

as : A unit vector to the motion of roller

- Omnidirectional property



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Locomotion Characteristics -7

Comments

- Stability of a vehicle is guaranteed with 3 wheels
 - Center of gravity is located within the triangle formed by ground contact points of the wheels
 - Stability is improved by 4 and more wheels
 - However, this arrangements are hyper-static and require a flexible suspension system
- Bigger wheels allow to overcome higher obstacles
 - Higher torque at wheel shaft is required
- Most arrangements are non-holonomic
 - Require high control effort
- Combining actuation and steering on one wheel makes the design complex and adds additional errors for odometry



Locomotion Characteristics -9

Non-Holonomic Systems

- Differential equations are not integrable to the final position
- The measure of the traveled distance of each wheel is not sufficient to calculate the final position of the robot
 - One has also to know how this movement was executed as a function of time



Some Robots -1

Synchro drive

- All wheels actuated synchronously by one motor
 - Defines the speed of the vehicle
- All wheels steered synchronously by a second motor
 - 。 Sets the heading of the vehicle
- Fixed orientation of the robot frame in world frame



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- Tribolo
 - An omnidirectional robot with 3 spherical wheels





□ A robot

An omnidirectional robot with 4 Swedish wheels



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(b) Three Sides Vi

) Three Sides



- □ Aim
 - Description of mechanical behavior of the robot for design and control
 - 。 Similar to manipulator kinematics
 - However, mobile robot can move unbounded with respect to its environment
 - There is no direct way to measure the robot's position
 - Position must be integrated over time
 - Leads to inaccuracies of the position (motion) estimates
 - The number 1 challenge in mobile robotics
 - Understanding mobile robot motion starts with understanding wheel constraints placed on the robots mobility

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- Kinematic model
 - Establish the robot speed $\xi = \begin{bmatrix} \dot{x} & \dot{y} & \dot{\theta} \end{bmatrix}_{i}^{T}$ as a function of the wheel speeds ϕ_{i_i} , steering angles β_i , steering speeds $\dot{\beta}_i$ and the geometric parameters of the robot (configuration coordinates)
 - Forward kinematics

$$\vec{\xi} = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{\theta} \end{bmatrix} = f(\phi_1, \dots \phi_n, \beta_1, \dots \beta_m, \dot{\beta}_1, \dots \dot{\beta}_m)$$

Inverse kinematics

 $\begin{bmatrix} \dot{\phi}_1 & \cdots & \dot{\phi}_n & \beta_1 & \cdots & \beta_m & \dot{\beta}_1 & \cdots & \dot{\beta}_m \end{bmatrix}^T = f(\dot{x}, \dot{y}, \dot{\theta})$



Mobile Robot Kinematics -3

 FYI: Manipulator Kinematics
 Forward kinematics of manipulators Given θ_i in ^w_iT, calculate ^w{H} or ^wP
 ^w_HT = f(θ₁,...,θ_i,...,θ_n)
 ^wP = ^w_iT ⁱP, i = 1,...,n
 Inverse kinematics – This chapter Given ^w{H} or ^wP, calculate θ_i in ^w_iT

 $[\theta_1, \dots, \theta_i, \dots, \theta_n] = f^{-1} \binom{w}{H} T$

 $\{H\}$

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Mobile Robot Kinematics -4 Representing robot position Initial frame $\{X_I, Y_I\}$ Robot frame $\{X_R, Y_R\}$ Robot position $\xi_I = \begin{bmatrix} x & y & \theta \end{bmatrix}^T$ Mapping between two frames $\xi_R = R(\theta)\xi_I = R(\theta) \cdot \begin{bmatrix} \dot{x} & \dot{y} & \dot{\theta} \end{bmatrix}^T$ $R(\theta) = \begin{bmatrix} \cos\theta & \sin\theta & 0\\ -\sin\theta & \cos\theta & 0\\ 0 & 0 & 1 \end{bmatrix}$





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- Assumptions
 - Movement on a horizontal plane
 - Point contact of the wheels
 - Wheels not deformable
 - Pure rolling
 - v = 0 at contact point



- No slipping, skidding or sliding
- No friction for rotation around contact point
- Steering axes orthogonal to the surface
- Wheels connected by rigid frame (chassis)









Spherical Wheel



- Given a robot with M wheels
 - Only fixed and steerable standard wheels impose constraints
 - Others impose zero constraints
- Suppose we have a total of $N = N_f + N_s$ standard wheels
 - Equations for the constraints in matrix forms
 - Rolling

$$J_1(\beta_s)R(\theta)\xi_I - J_2\phi = 0 \qquad \varphi(t) = \begin{bmatrix} \varphi_f(t) \\ \varphi_s(t) \end{bmatrix} \qquad J_1(\beta_s) = \begin{bmatrix} J_{1f} \\ J_{1s}(\beta_s) \end{bmatrix} \qquad J_2 = diag(r_1 \cdots r_N)$$

Sliding

$$C_1(\boldsymbol{\beta}_s)R(\boldsymbol{\theta})\boldsymbol{\xi}_I = 0 \qquad C_1(\boldsymbol{\beta}_s) = \begin{bmatrix} C_{1f} \\ C_{1s}(\boldsymbol{\beta}_s) \\ (N_f + N_s) \leq 3 \end{bmatrix}$$

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Wheel Kinematic Constraints -6 • Example: Differential Drive Robot • Rolling constraint $[\sin(\alpha + \beta) - \cos(\alpha + \beta) (-l)\cos\beta]R(\theta)\dot{\xi}_l - r\dot{\phi} = 0$ • Sliding constraint $[\cos(\alpha + \beta) \sin(\alpha + \beta) l\sin\beta]R(\theta)\dot{\xi}_l = 0$ • Forward direction = X_R • Right wheel: $\alpha = -\frac{\pi}{2} \beta = \pi$ • Left wheel: $\alpha = \frac{\pi}{2} \beta = 0$

Constraints

Right wheel J:
$$\begin{bmatrix} 1 & 0 & l \end{bmatrix} R(\theta) \dot{\xi}_{l} - r_{r} \dot{\varphi}_{r} = 0$$

Left wheel J: $\begin{bmatrix} 1 & 0 & -l \end{bmatrix} R(\theta) \dot{\xi}_{l} - r_{l} \dot{\varphi}_{l} = 0$
 $C: \begin{bmatrix} 0 & 1 & 0 \end{bmatrix} R(\theta) \dot{\xi}_{l} - \begin{bmatrix} J_{2} \dot{\varphi} \\ 0 \end{bmatrix} = 0$
 $\begin{bmatrix} J_{1}(\beta_{s}) \\ C_{1}(\beta_{s}) \end{bmatrix} R(\theta) \dot{\xi}_{l} - \begin{bmatrix} J_{2} \dot{\varphi} \\ 0 \end{bmatrix} = 0$
 $\begin{bmatrix} 1 & 0 & l \\ 1 & 0 & -l \\ 0 & 1 & 0 \end{bmatrix} R(\theta) \dot{\xi}_{l} = \begin{bmatrix} \begin{bmatrix} r_{r} & 0 \\ 0 & r_{l} \end{bmatrix} \begin{bmatrix} \dot{\varphi}_{r} \\ \dot{\varphi}_{l} \end{bmatrix}$
 $\dot{\xi}_{l} = R(\theta)^{-1} \begin{bmatrix} \frac{1}{2} & \frac{1}{2} & 0 \\ 0 & 0 & 1 \\ \frac{1}{2l} & -\frac{1}{2l} & 0 \end{bmatrix} \begin{bmatrix} r_{r} & 0 \\ 0 & r_{l} \end{bmatrix} \begin{bmatrix} \dot{\varphi}_{r} \\ \dot{\varphi}_{l} \end{bmatrix} = \begin{bmatrix} \cos\theta & -\sin\theta & 0 \\ \sin\theta & \cos\theta & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \frac{r\dot{\varphi}_{r}}{2} + \frac{r\dot{\varphi}_{l}}{2} \\ \frac{r\dot{\varphi}_{r}}{2} - \frac{r\dot{\varphi}_{l}}{2l} \end{bmatrix}$
The same result, formal approach 39

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